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Application of density functional theory in studying $CO₂$ capture with TiO₂supported K_2CO_3 being an example

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Qi[a](#page-0-0)oyun Qin^{a[,1](#page-0-1)}, Hongyan Liu^{a[,b,](#page-0-2)[1](#page-0-1)}, Riguang Zhang^{a,[c](#page-0-3)}, Lixia Ling^a, Maohong Fan^{[c,](#page-0-3)}*, Baojun Wang^{[a,](#page-0-0)}*

a Key Laboratory of Coal Science and Technology of Ministry of Education and Shanxi Province, Taiyuan University of Technology, Taiyuan, Shanxi 030024, China ^b College of Chemistry and Environmental Engineering, Shanxi Datong University, Datong, Shanxi 037009, China

^c Departments of Chemical and Petroleum Engineering, University of Wyoming, Laramie, WY 82071, USA

HIGHLIGHTS

GRAPHICAL ABSTRACT

- Preadsorbed H_2O makes CO_2 adsorption increase over K_2CO_3/TiO_2 sorbent.
- \bullet CO₂ and H₂O prefer to adsorb at the interface of K_2CO_3/TiO_2 .
- Carbonation reaction is governed by H₂O dissociation.
- \bullet The better K-based sorbent for CO₂ capture is proposed.

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ABSTRACT

Solid sorbents based CO₂ capture has become increasingly important. Great progress has been achieved with experimental studies in this area. However, the density functional theory based capture study on the function of $H₂O$ in CO₂ capture is lacking. This research was designed to make progress in this important area with TiO₂supported K_2CO_3 being an example. Due to its high cost-effectiveness, dry K_2CO_3 is a promising sorbent for capturing CO2. Yet challenges remain in accelerating the rate of the absorption process. The study of mechanism of the effect of H_2O on CO_2 adsorption as well as the carbonation reaction can help select and design better support for the sorbent. Up to now, it is open. In this work, the adsorption and reaction of CO_2 over K_2CO_3 loaded on a rutile (1 1 0) surface have been studied using theoretical calculations. The results show that the $CO₂$ adsorption is increased when H₂O appears, and carbonation reaction mainly occurs at the interfaces of K₂CO₃/ TiO₂ includes bicarbonate formation resulting from the reactions of CO₂ with OH via H₂O dissociation and CO₃ anion with transferred H via H₂O dissociation combining. In addition, H transfer step appears when support TiO₂ exists compared to that on pure K_2CO_3 sorbent. The kinetic modeling indicates that the H₂O dissociation may limit the carbonation reaction. Therefore, H_2O -dissociative or high OH coverage TiO₂ support material can assist $CO₂$ sorption with the solid K₂CO₃ based CO₂ capture technology. It is expected that the theoretical study sheds light on the preparation of cost-effective $CO₂$ sorbents in the future.

⁎ Corresponding authors.

 $^{\rm 1}$ The two authors have equal contribution to the paper.

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E-mail addresses: mfan@uwyo.edu (M. Fan), wangbaojun@tyut.edu.cn (B. Wang).

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1. Introduction

Global warming caused by greenhouse gas emission has, in recent years, been recognized as a major risk to mankind [\[1](#page-11-0)–3]. Carbon dioxide $(CO₂)$ is one of the major greenhouse gases, and it has been reported that one-third of $CO₂$ emissions worldwide come from fossil fuelbased power plants $[4]$. Hence, capturing $CO₂$ emitted from the flue gas of power plants has been considered to be a potentially effective approach to controlling atmospheric CO₂ levels.

Methods explored to remove $CO₂$ from flue gas include membrane separation (separated CO_2 from a CO_2-N_2 mixed gas) [\[5\],](#page-11-2) absorption with a solvent $(CO₂$ absorption with aqueous, blends of monoethanolamine and N-methyldiethanolamine, etc.) [\[6,7\]](#page-11-3), and adsorption on molecular sieves (adsorption–desorption on molecular sieves by pressure or temperature swing) [\[8,9\]](#page-11-4). However, these methods are costly and consume large amounts of energy. One of the improved techniques for the removal of $CO₂$ is the chemical absorption of $CO₂$ with dry renewable K_2CO_3 sorbents [\[10,11\]](#page-11-5) and K_2CO_3 -promoted hydrotalcite sorbents [\[12,13\]](#page-11-6). Hydrotalcites have the unique property of $CO₂$ sorption at high temperatures (200–600 °C), which can be applied to the direct $CO₂$ removal from flue gases without cooling process. The equilibrium $CO₂$ sorption uptake of hydrotalcite could be much more increased by impregnation with K_2CO_3 . However, the regeneration temperature is high. Meanwhile, K_2CO_3 sorbents are employed in CO_2 absorption from flue gas of fossil-fueled based thermal power plants at low temperatures (50–90 °C). The use of K_2CO_3 sorbents can be highly cost effective and an energy efficient way to remove $CO₂$ from flue gas following the reaction $K_2CO_3 + CO_2 + H_2O \leftrightarrow 2KHCO_3$. In addition, the global carbonation reaction rate for pure K_2CO_3 is rather slow [\[14\]](#page-11-7). We therefore suggested that, in preparation support, a promoter or special technique may be needed to modify the structure of the K_2CO_3 surfaces to strengthen the adsorption of CO₂, thereby further improving conversion of carbonate to the bicarbonate based our theoretical calculation.

Some supports such as SiO_2 , Al_2O_3 , CaO, MgO, TiO₂ and activated carbon (AC) have been used in alkali metal-based sorbents to enhance $CO₂$ capture. Lee et al. $[15-18]$ $[15-18]$ and Zhao et al. $[19-22]$ $[19-22]$ found that sorbents of K₂CO₃/AC, K₂CO₃/TiO₂, K₂CO₃/MgO, and K₂CO₃/Al₂O₃ showed excellent $CO₂$ capture capacity; on the other hand, those sorbents were completely regenerated above 130, 130, 350, and 400 °C, respectively. However, the $CO₂$ capture capacities of $K₂CO₃/Al₂O₃$ and K2CO3/MgO decreased during multiple absorption/regeneration cycles (absorption at 60 °C and regeneration at 150 °C), mainly due to the formation of KAl(CO₃)₂(OH)₂, K₂Mg(CO₃)₂, and K₂Mg(CO₃)₂·4(H₂O), which did not completely convert to the original K_2CO_3 phase. However, unlike K_2CO_3/Al_2O_3 and K_2CO_3/MgO , a KHCO₃ crystal structure was formed during CO_2 absorption on K_2CO_3/AC and K_2CO_3/TiO_2 sorbent. This phase could easily be converted into the original phase during regeneration, even at a low temperature (130 °C). Meanwhile, Lee et al. [\[23\]](#page-11-10) investigated the structure effects of potassium-based $\rm TiO_2$ (anatase) sorbents on $\rm CO_2$ capture capacity. Under the temperature of calcine, the $CO₂$ capture capacity of the sorbent was reduced due to the undesired formations of $K_2Ti_2O_5$, $K_2Ti_6O_{13}$, and $K_2Ti_4O_9$. However, the rutile structure of $TiO₂$ can prevent the formation of new structures such as $K_2Ti_2O_5$ and $K_2Ti_6O_{13}$, thus significantly affect CO_2 capture capacity. In addition, $TiO(OH)_2$ has been found to be a promising catalytic support for not only improving $CO₂$ capture of solid sorbents [\[24,25\]](#page-11-11), but dramatically reducing energy consumption [\[26\]](#page-11-12).

The reaction mechanism for CO_2 uptake by K_2CO_3 and the role of $H₂O$ in the reaction are open. Mahinpey et al. [\[27\]](#page-11-13) reported that $K₂CO₃$ hydration to form $K_2CO_3 \cdot 1.5H_2O$ and carbonation occur in parallel, without direct conversion from $K_2CO_3·1.5H_2O$ to KHCO₃. Further, Mahinpey et al. [\[28\]](#page-11-14) discussed the kinetic behavior of solid K_2CO_3 under $CO₂$ capture and brought up that the carbonation reaction are limited by adsorption, not chemical reaction based on proposed Langmuir-Hinshelwood model. However, Zhao et al. [\[29\]](#page-11-15) and Li et al. [\[30\]](#page-11-16)

suggested that $K_2CO_3 \cdot 1.5H_2O$ can react with CO_2 in a fast kinetic rate. Meanwhile, Li et al. [\[31\]](#page-11-17) determined that hydration reaction occurred through the reaction between K_2CO_3 and the steam, and approximately 75% of K_2CO_3 were converted to K_2CO_3 1.5H₂O in high temperature, however, $KHCO₃$ cannot directly react with the steam to produce $K_2CO_3·1.5H_2O$. Although there have been some experimental explorations into the mechanism of carbonation reaction, it is difficult to understand the mechanism completely due to the complexity of $CO₂$ capture with K_2CO_3 sorbent. Quantum mechanics calculation is a useful tool to help clarify the detail of the reaction. Gao et al. [\[32\]](#page-11-18) investigated the carbonation reaction only on pure K_2CO_3 with monoclinic structure using the density functional theory (DFT) method, proposing that the carbonation reaction occurs via the single "one-step mechanism", i.e., the OH group resulting from the dissociation of H_2O attacking the C of $CO₂$ to form bicarbonate. Also, the same reaction on low index surfaces of pure K_2CO_3 with both cubic and monoclinic structures was studied, and it was confirmed that the carbonation reaction can directly proceed either via the interaction between OH resulting from H_2O dissociation and the C atom of $CO₂$ on monoclinic and hexagonal $K₂CO₃$, or between the OH group from H_2O dissociation reacting and gaseous CO_2 on hexagonal K_2CO_3 , i.e., the carbonation reaction is both a "one-step" and a "two-step mechanism" $[14]$. Further, investigating the $CO₂$ desorption reaction on an anatase-TiO₂ (101) surface by DFT method, Wu et al. [\[33\]](#page-11-19) concluded that the formation of the unstable intermediary TiO (OH)⁺ and OH[−] by the adsorption of H₂O on the catalyst TiO₂ surface can accelerate the reaction. However, in their work the initial states are not KHCO₃, but rather hydroxyl and carbonyl states. On the other hand, adsorption and carbonation of $CO₂$ and $H₂O$ on pure rutile or anatase have been investigated extensively. For instance, investigating the coadsorption properties of $CO₂$ and $H₂O$ on rutile of TiO₂ (110) using a dispersion-corrected DFT study, Sorescu et al. [\[34\]](#page-11-20) found that the coadsorbed H_2O or OH species slightly increase the CO_2 adsorption energies. Other influence factors, including the solvent effect [\[35\]](#page-11-21) and the effect of excess electron and hole [\[36\],](#page-11-22) have also been investigated. However, CO_2 captured by TiO₂-supported K_2CO_3 sorbent still has not been investigated using a theoretical method. Does $TiO₂$ -supported K_2CO_3 capture CO_2 better than pure K_2CO_3 or clean TiO₂? What is the capture mechanism in detail? Where is the active site? The above questions are open.

In order to increase $CO₂$ capture efficiency, it is imperative to make clear the mechanism by which K_2CO_3/TiO_2 captures CO_2 . This work focuses mainly on the mechanisms of the K_2CO_3/TiO_2 (rutile) capture of $CO₂$ through DFT calculation, due to the relatively simpler capture/ regeneration mechanism on rutile-supported K_2CO_3 than other media. At the same time, the results are compared with those using pure K_2CO_3 or clean TiO₂ so that the CO₂ capture mechanism can be comprehended better.

2. Computational details

2.1. Computational methods

The DFT approach has been proved to be very successful in modeling the ground state properties of various structures, and has thus been widely used to predict the structural and energetic properties. DFT with Hubbard U correction is to treat the strong on-site Coulomb repulsion, which is not correctly described by LDA or GGA, mainly employed to calculate and analysis the refined electronic structures. At present, geometric optimization and transition state search cannot yet be carried out using the DFT+U method in the CASTEP code, largely because DFT alone has been considered fairly reliable in most cases for structural optimization, resulting in lattice parameters below 1% level of inaccuracy [\[37,38\].](#page-11-23)

Previous experimental and theoretical studies have demonstrated that $CO₂$ molecules interact relatively weakly with the rutile(1 1 0) and K_2CO_3 surface. Thus, one might presume that long-range dispersion interactions would be important for characterizing the $CO₂$ -surface interactions.

In this study, DFT calculations were performed to measure $CO₂$ and H2O adsorption and carbonate formation processes on the surface of K_2CO_3 loading on TiO₂ using periodic slab models [39–[42\].](#page-11-24) All calculations were performed using the Cambridge Sequential Total Energy Package (CASTEP) [\[38\]](#page-11-25) of Materials Studio 8.0 from Accelrys with the General Gradient Approximation (GGA) Perdew-Wang 1991 (PW91) functional [\[43\]](#page-11-26); the pseudo potential is ultrasoft. The DFT-D3 correction [\[44\]](#page-11-27) was incorporated with the PW91 functional to handle dispersion interaction, and a large convergence of the plane wave expansion was obtained with an energy cutoff of 340 eV. For geometry optimization, the Brillouin zone was sampled in a $2 \times 2 \times 1$ Monkhorst-Pack set [\[45\].](#page-11-28) The geometries were not optimized until the energy, force and max displacement converged to 2.0×10^{-5} eV/atom, 0.05 eV/Å and 2×10^{-3} Å, respectively. Useful thermodynamic data can be calculated based on calculation of the phonon frequencies.

Before adspecies adsorption, the binding energy of K_2CO_3 and TiO_2 , was evaluated according to the following formula:

$$
E_{\rm b} = E_{\rm (K_2CO_3/TiO_2)} - E_{\rm (K_2CO_3)} - E_{\rm (TiO_2)} \tag{1}
$$

where $E_{(K_2CO_3/TiO_2)}$ is the total energy of the whole system when K_2CO_3 is deposited on TiO₂, $E_{(K_2CO_3)}$ is calculated by putting a K_2CO_3 unit in a $10 \text{ Å} \times 10 \text{ Å} \times 10 \text{ Å}$ box, and $E_{\text{(TiO}_2)}$ is the energy of clean TiO₂ (1 1 0) slab.

The adsorption energy is evaluated according to the following formula:

$$
E_{\text{ads}} = E_{\text{(adsorbate/K}_2\text{CO}_3/\text{TiO}_2)} - E_{\text{(K}_2\text{CO}_3/\text{TiO}_2)} - E_{\text{(adsorbate)}} \tag{2}
$$

where $E_{(adsorbate/K_2CO_3/TiO_2)}$ is the total energy of the surface of K₂CO₃/TiO₂ with adsorbate; $E_{\text{(adsorbate)}}$ is the energy of the free adsorbate $(H_2O$ or $CO_2)$, which is calculated by putting adsorbate in a $10 \text{ Å} \times 10 \text{ Å} \times 10 \text{ Å}$ box; And $E_{(K_2CO_3/T_1O_2)}$ is the total energy of K_2CO_3 supported on $TiO₂$.

The adsorption energy of $CO₂$ co-adsorption with other species is defined as:

$$
E_{\rm co-ads} = E_{\rm (CO_2/H_2O/K_2CO_3/TiO_2)} - E_{\rm (H_2O/K_2CO_3/TiO_2)} - E_{\rm (CO_2)}
$$
(3)

where $E_{\text{(CO}_2/H_2\text{O/K}_2\text{CO}_3/\text{TiO}_2)}$ is the total energy of the surface of K₂CO₃/ TiO₂ with adsorbates H₂O and CO₂, $E_{(H_2O/K_2CO_3/TiO_2)}$ is the total energy of the surface of K_2CO_3/TiO_2 only with adsorbate H_2O , and $E_{(CO_2)}$ is the energy of the free CO₂ obtained by putting CO₂ in a 10 Å \times 10 Å \times 10 Å box.

The standard molar Gibbs free energy for gaseous species and ad-sorbed species can be calculated using the following formula [\[46\]](#page-11-29):

$$
G^{\theta}(T, p) = E_{\text{total}} + E_{ZPE} + U^{\theta} - TS^{\theta} + \gamma RT \left[1 + \ln \left(\frac{p}{p^{\theta}} \right) \right]
$$
(4)

$$
U_{Vib}^{\theta} = RT \sum_{i} \frac{hv_i/k_B T}{e^{hv_i/k_B T} - 1}
$$
\n(5)

$$
S^{\theta} = R \sum_{i=1}^{n} -\ln(1 - e^{hw_i/k_B T}) + \frac{hv_i/k_B T}{e^{hw_i/k_B T} - 1}
$$
(6)

where E_{total} refers to the total energy obtained directly from DFT calculations, R is the gas constant, p is the partial pressure of the gas-phase molecules, and γ is 0 for surface adsorbed species, and 1 for gaseous molecule; E_{ZPE} is the zero-point vibrational energy; U^{θ} and S^{θ} are the thermal energy and entropy, respectively.

In addition, the activation energy E_a and reaction energy ΔE are calculated according to the following formula:

$$
E_{\rm a} = E_{\rm TS} - E_{\rm R} \tag{7}
$$

$$
\Delta E = E_{\rm P} - E_{\rm R} \tag{8}
$$

where E_R , E_{TS} and E_P are the energies of reactants, transition states and

products in an elementary reaction, respectively.

The reaction rate constants (k) can be obtained using harmonic transition state theory [\[47\]:](#page-11-30)

$$
k = \frac{k_{\rm B} T}{h} \frac{q_{\rm TS}}{q_{\rm R}} \exp(-\frac{E_{\rm act}}{k_{\rm B} T})
$$
\n(9)

$$
q = \frac{1}{\prod_{i=1}^{\text{Vibration}} 1 - \exp(-\frac{hv_i}{k_B T})}
$$
(10)

where k_B is the Boltzmann constant, T is the actual temperature (350 K), and E_{act} represents the DFT-calculated and zero-point-corrected activation energy.

2.2. Computational model

Unlike a sorbent prepared using anatase structure $TiO₂$. Lee et al. [\[23\]](#page-11-10) determined that sorbent prepared by impregnating $TiO₂$ having a rutile structure with 30% K₂CO₃ is of the constant capacity of $CO₂$ capture. Additionally, it is easy to regenerate K_2CO_3 supported by TiO₂ with rutile structure after $CO₂$ capture. Therefore, rutile is considered as the support in this work.

The crystallographic data for rutile bulk structure used in this work was taken from the Inorganic Crystal Structure Database (ICSD-200391). The structure was subsequently geometrically optimized (energy minimization) to test the methods used in this work, and the calculated lattice parameters of bulk rutile are $a = 4.646 \text{ Å}$ and c / $a = 0.637 \text{ Å}$, which are in good agreement with the experimental results of a = 4.594 Å and $c/a = 0.644$ [\[48\]](#page-11-31) (i.e., the deviations are only 1.13% and 1.08%, respectively). This indicates that the employed method is suitable for carrying out the calculations in this work.

Being of the minimal energy, (1 1 0) surface of rutile is preferentially expressed in macroscopic crystal morphologies, and has been assumed to dominate the surface chemistry [\[49\].](#page-11-32) Herein, a (4 \times 2) supercell was used to represent rutile $TiO₂(1 1 0)$ containing five layers, with the bottom two layers kept frozen at bulk optimized positions and the upper three layers allowed to relax. Vacuum thickness (size of unit cell perpendicular to slab-slab thickness) was set to be 15 Å, which is large enough to avoid unnecessary potential surface-surface interaction. The electrons transfers were also calculated for comparison through Mulliken population analysis.

For the computational model, a K_2CO_3 monomer supported on the rutile (1 1 0) surface was used to represent the active component of K_2CO_3 deposited on TiO₂, in which the structure of K_2CO_3 is composed of nearly planar CO₃ anions and K cations coordinated to oxygen atoms.

3. Results and discussion

3.1. TiO₂ supported K_2CO_3

There are three types of surface structures for carbonate anion deposited on oxide, i.e., bidendate, mondendate and bridge structures [\[50\]](#page-11-33); the position of the K species on the TiO₂ (1 1 0) is between the bridging oxygen [\[51\]](#page-11-34). Based on the above position and surface structures, the possible configurations of K_2CO_3 deposited on TiO₂(110) were explored, and the results showed that carbonate anion of K_2CO_3 favors binding on the surface of $TiO₂$ in bridge structure, i.e., the two O atoms from carbonate bind with two Ti atoms of surface. The distances are 1.967 and 1.969 Å, respectively, and the distances of K cations and O atoms of the surface are 2.589 and 2.800 Å, respectively [\(Fig. 1\)](#page-3-0). The calculated binding energy is $-711.1 \text{ kJ} \text{ mol}^{-1}$, indicating that K₂CO₃ is bound substantially stronger on TiO₂ (1 1 0).

We also performed PDOS analysis for the supported configurations ([Fig. 2](#page-3-1)). There are many resonance peaks between s-, p-from O in K_2CO_3 and s-, p-, d-from Ti, confirming strong interaction between K_2CO_3 and $TiO₂$ support, which indicating that the new phase is not easy to form in the calcination process. This is consistent with the experimental results

Fig. 1. The main model of K_2CO_3 loaded on (4×2) rutile of TiO₂ (100) surface.

Fig. 2. PDOS plots for K_2CO_3 deposit on TiO₂ (110) surface. (O from K_2CO_3 and Ti from $TiO₂$).

[\[23\]](#page-11-10) that sorbent prepared by impreganation of $TiO₂$ having the rutile structure almost did not transform into new structure such as $K_2Ti_2O_5$ and $K_2Ti_6O_{13}$ below 500 °C.

3.2. $CO₂$ and H₂O adsorption

For the K₂CO₃ loaded on (4 \times 2) rutile (1 1 0) surface, investigation of the adsorption of CO_2 and $\mathrm{H}_2\mathrm{O}$ on the surface is lacking. Here, stable adsorption configurations were found, marked as $C(1)$ – $C(4)$ for $CO₂$ adsorption, $W(1)$ – $W(2)$ for $H₂O$ molecular adsorption, and $DW(1)$ – DW (2) for $H₂O$ dissociative adsorption [\(Fig. 3\)](#page-4-0). The corresponding adsorption energies and structural parameters, as well as Mulliken charges, are listed in [Table 1.](#page-4-1)

3.2.1. $CO₂$ adsorption

For $CO₂$ adsorption, there are four different binding configurations of CO_2 on K_2CO_3 loaded on TiO₂ (1 1 0) surface. In C(1) and C(2), the $CO₂$ molecule is adsorbed at the interface of $K₂CO₃$ and TiO₂, in which an O atom from adsorbed $CO₂$ is located above a Ti site, and the whole CO2 maintains a linear configuration, tilting relative to the surface normally toward a nearby bridge O site on the $TiO₂$ surface. The distances of Ti and the O of CO_2 are 2.755 and 2.809 Å, and the distances of K and the nearest neighboring O of $CO₂$ are 2.873 and 3.003 Å, respectively. The adsorption energies are -43.4 and -40.5 kJ·mol $^{-1}$, respectively. In $C(3)$ and $C(4)$, the $CO₂$ molecule is adsorbed on the support $TiO₂$. $CO₂$ is adsorbed along the Ti row in a lying-down configuration in C(3) with the adsorption energy of $-31.8 \text{ kJ·mol}^{-1}$. Meanwhile, $CO₂$ is adsorbed on the top of the bridge oxygen atom rather than in the middle of two bridge oxygen atoms in C(4), with the

adsorption energy of $-23.2 \text{ kJ} \text{ mol}^{-1}$. Analyzed by the Mulliken charge, it is found that there are a few electrons transferred from the interface of K_2CO_3/TiO_2 as well as the surface of TiO₂ to the CO₂, which changes the $C-O$ bond slightly.

The adsorbed configurations discussed above are similar to those of $CO₂$ adsorbed on TiO₂ (1 1 0) with or without the H₂O environment obtained by Liu et al. [\[35\].](#page-11-21) However, the adsorption energies are larger than those on pure TiO₂ (1 1 0), but smaller than those on TiO₂(1 1 0) with H₂O solvent effect and pure K_2CO_3 [\[14\].](#page-11-7) In order to compare the effect of the K_2CO_3/TiO_2 interface on the adsorption of CO_2 , we also investigated the adsorption of CO_2 on clean TiO₂ (1 1 0). After removing the K_2CO_3 from TiO₂, there are three configurations for the adsorption of $CO₂$ on TiO₂ (1 1 0) corresponding to C(1), C(3) and C(4) in [Fig. 3](#page-4-0) (note: C(1) is equal to C(2) in such a case). The calculated adsorption energies are -33.8 , -32.8 and -23.2 kJ·mol⁻¹ on clean TiO₂ (1 1 0) surface, respectively. The results are almost consistent with our adsorption energies obtained with $CO₂$ adsorbed on the support $TiO₂$ of K_2CO_3/TiO_2 , but lower than that with CO_2 adsorbed at the interface of K_2CO_3/TiO_2 . Therefore, we will use the results from the support TiO₂ of K_2CO_3/TiO_2 instead of those from pure TiO₂ in the following study. In addition, our calculated results about $CO₂$ adsorbed on rutile (110) surface with DFT-D3 are almost in agreement with those by Sorescu et al. [\[34\],](#page-11-20) whose results are -42.5 , 37.6 and -21.2 kJ·mol⁻¹ using DFT+U method. This can further confirm that DFT-D3 method also is suitable for carrying out the calculation to investigate the geometry and reaction process in this work.

On the other hand, the heat of adsorption, which is a measure of the energy required for regeneration, should be substantially low. Heats of adsorption are generally in the range of -25 to -50 kJ·mol⁻¹ for physisorption cases [\[52\]](#page-11-35). Interestingly, our calculated adsorption energies of CO₂ are -23.2 to -43.4 kJ·mol⁻¹, which is consistent with the experimental results. The identical results guarantee the confidence of our calculated data.

3.2.2. $H₂O$ adsorption

3.2.2.1. Molecular adsorption. There are two different binding configurations of H₂O over K₂CO₃ loaded on TiO₂ (110) surface. In the most stable adsorption configuration, $W(2)$, the O atom of the H_2O molecule interacts with a surface Ti atom and a K cation, and forms a hydrogen bond to a surface O_b atom; the adsorption energy of this configuration is $-98.4 \text{ kJ·mol}^{-1}$. However, in the other adsorption configuration, $W(1)$, the O atom of the H₂O molecule interacts only with a surface Ti atom and forms a hydrogen bond to a surface O_b atom; the adsorption energy of this configuration is -81.0 kJ·mol−¹ , which is smaller than that in W(2) due to less interaction with the K_2CO_3 . Obviously, H_2O prefers to adsorb at the interface between K_2CO_3 and $TiO₂$ in W(2) than on the surface of support $TiO₂$ in W(1). It has been found that the adsorption energy of H_2O over K_2CO_3 deposited on TiO₂ (1 1 0) surface is a little stronger than that on TiO₂ (1 1 0) by Bandura et al. [\[53\],](#page-11-36) who obtained the adsorption energy of $-92.0 \text{ kJ·mol}^{-1}$. Those are stronger than the result obtained by Sahoo et al. [\[54\],](#page-11-37) which showed the binding strength of H₂O of 60.8 kJ·mol⁻¹. In addition, the adsorption of H₂O on pure K₂CO₃ up to 126.4 kJ·mol⁻¹ [\[14\]](#page-11-7) is stronger than that at the interface of K_2CO_3/TiO_2 and support of TiO₂.

3.2.2.2. Dissociative adsorption. In recent studies, it was found that H_2O molecules not only remain intact when adsorbed at low temperature at monolayer coverage, but also that a small portion of H_2O monomers can dissociate, with the fraction of such dissociated monomers increasing with increased temperature [\[55,56\]](#page-11-38). Accordingly, we also investigated the dissociative adsorption of H_2O on K_2CO_3/TiO_2 . Starting from the stable adsorption of $H₂O$ on the sorbent with the configurations of $W(1)$ and $W(2)$, the dissociated H_2O molecule leads to formation of a terminal hydroxyl (marked as OH_t , adsorbed on the top of Ti) and a bridging hydroxyl (marked as OH_b , in which O is from TiO₂, which expresses that H_b is adsorbed on O). The distances between the H

Fig. 3. Top views of the main adsorption configurations of CO₂ and H₂O on the K₂CO₃-loaded TiO₂ (1 1 0) surface [configurations C(1)–C(4) for CO₂ adsorption; configurations W(1) and W(2) for H₂O molecular adsorption; configurations DW(1) and DW(2) for H₂O dissociative adsorption]. For increased clarity, the oxygen atoms of CO₂ and H₂O are indicated in pink, and the oxygen atoms of the slab are indicated in red. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

in OH_b and the O atom in OH_t are 2.431 and 2.259 Å in DW(1) and DW (2), and the adsorption energies of $H₂O$ are −70.4 and −117.7 kJ·mol−¹ , respectively.

Whether H_2O is adsorbed in the form of molecule or dissociation, the interaction between H_2O and the K_2CO_3 loaded on TiO₂ (110) surface is much stronger than that between $CO₂$ and the $K₂CO₃$ loaded on TiO₂ (1 1 0) surface. This implies that when H_2O is adsorbed firstly on the TiO₂ (1 1 0) surface, CO_2 molecules will not be able to displace the adsorbed $H₂O$ molecules. This finding suggests that pre-adsorbed $H₂O$ blocks CO₂ adsorption, and it is consistent with the results on pure $TiO₂(1 1 0)$ obtained by Henderson et al. [\[57\]](#page-11-39) and Sorescu et al. [\[34\]](#page-11-20).

3.3. $CO₂$ -H₂O co-adsorption

Because the adsorption of H_2O is far stronger than that of CO_2 , when $CO₂$ is being captured, pre-adsorbed H₂O has an effect on $CO₂$ adsorption that cannot be ignored in the process. Therefore, the coadsorption of $CO₂-H₂O$ needs to be investigated.

3.3.1. $CO₂$ and molecular H₂O co-adsorption

We considered co-adsorption of H_2O with a CO_2 molecule on K2CO3/TiO2, based on the aforementioned four-adsorption configuration of CO₂. The largely CO₂-H₂O configurations are marked as M(1)-M (4), shown in [Fig. 4,](#page-5-0) and the corresponding adsorption energies, structural parameters, and Mulliken charges are given in [Table 2](#page-5-1).

For all co-adsorption configurations, M(1), M(3) and M(4) represent $CO₂$ adsorbed on a Ti site based on the W(2) structure of H₂O adsorption on a TiO₂ surface; meanwhile, M(2) expresses $CO₂$ adsorbed on a Ti site based on the W(1) structure of H_2O adsorption at the interface of K_2CO_3/TiO_2 . These adsorbed configurations cause the formation of a hydrogen bond between the H2O molecule and one of the O atoms of $CO₂$, with the bond angle of the $CO₂$ molecule being slightly decreased, which leads to a slight increase in $CO₂$ adsorption energy. The adsorption energies of M(1), M(2), M(3) and M(4) are increased by 1.9,

Table 1

Adsorption energies, representative geometrical parameters, and Mulliken charge of CO₂ and H₂O molecules adsorbed at different sites on K₂CO₃ loaded on TiO₂ (1 1 0) surface.

Configurations	r(Ti-O _c) ^a (Å)	$r(C-Ob)b (Å)$	$r(K-Oc)a$ (Å)	$r(C-O)$ (A)	α (OCO) (\degree)	E_{ads} (kJ·mol ⁻¹)	Charge (e)
CO ₂ (gas)				1.184, 1.184	180.0		
C1	2.755	2.927	2.873	1.176, 1.183	177.2	-43.4	-0.03
C ₂	2.809	2.958	3.003	1.176, 1.186	176.4	-40.5	-0.07
C ₃	2.763, 2.999	$-$	4.986	1.181, 1.182	178.6	-31.8	-0.05
C ₄	$\overline{}$	2.655	4.405	1.180, 1.185	176.2	-23.2	-0.06
Configurations	r(Ti-O _w) ^c (Å)	$r(O_b-H)^c$ (Å)	$r(K-O_w)^c$ (Å)	r(O _w -H) ^c (Å)	$\alpha(HO_wH)$ (°)	E_{ads} (kJ·mol ⁻¹)	Charge (e)
H ₂ O(gas)				0.979, 0.979	104.2		
W1	2.355	1.916	$\overline{}$	0.975, 0.999	109.2	-81.0	0.03
W ₂	2.538	2.735	2.711	0.980, 0.988	104.2	-98.4	0.02
DW(1)	1.842	0.981	$\overline{}$	0.978, 2.257	$\overline{}$	-70.4	0.04
DW(2)	1.903	0.981	2.632	0.977, 2.431	$\qquad \qquad$	-117.7	-0.06

^a The O_c is refer to O atom of CO₂ molecule.
^b The O_b is refer to a generic surface bridging O atom. ^c The O_w is refer to O atom of H₂O molecule.

Fig. 4. Top views of the main co-adsorption configurations of CO₂ and H₂O species over the K₂CO₃ loaded on rutile (110) surfaces. For increased clarity, the oxygen atoms of CO₂ and H₂O are indicated in pink, and the oxygen atoms of the slab are indicated in red. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

17.4, 8.7 and 18.3 kJ·mol⁻¹, respectively. Certainly, the smallest increase from $C(1)$ to $M(1)$ it is for these co-adsorption configurations, while the biggest increment it is from $C(4)$ to $M(4)$. Sorescu et al. [\[34\]](#page-11-20) concluded that the largest enhancement of the $CO₂$ adsorption energy may be observed for configurations that are most weakly bound to the surface in the absence of $H₂O$, which is consistent with our findings. In addition, the presence of the H_2O molecule may increase the adsorption stability of the CO_2 molecule. Even if the co-adsorption of H_2O with $CO₂$ makes the adsorption of $CO₂$ increase in the above four cases, the most stable co-adsorption configuration of $CO₂$ with H₂O is $CO₂$ adsorption at the interface of K_2CO_3/TiO_2 with M(2) configuration. In addition, the adsorption energy increments of $CO₂$ is larger on $K₂CO₃/$ TiO₂ (1 1 0) than those on pure TiO₂ (1 1 0) [\[34\]](#page-11-20). Liu et al. [\[35\]](#page-11-21) also found that the co-adsorbed H_2O can increase the binding energy of CO_2 by 6.1 to 11.6 kJ·mol−¹ in both the vacuum and solvent cases.

3.3.2. $CO₂$ and dissociative H₂O co-adsorption

Because adsorbed H_2O molecules can dissociate to form OH_t and OH_b species, we need to consider the interaction of $CO₂$ with the two types of hydroxyl groups when studying the co-adsorption of $CO₂$ and $H₂O$ molecules on a $K₂CO₃$ -loaded TiO₂ (1 1 0) surface. Starting from relatively stable adsorption configurations of $CO₂$, we have also analyzed the co-adsorption of a $CO₂$ molecule over $K₂CO₃$ loaded on a (4×2) TiO₂ (1 1 0) surface with terminal OH_t and bridging OH_b species, as well as with H. The corresponding co-adsorption configurations, denoted DA(1)–DA(4), are shown in [Fig. 5](#page-6-0); the corresponding adsorption energies (E_{ads}) and structural parameters as well as Mulliken charges, are given in [Table 3](#page-6-1).

Similar to the case with $CO₂$ and $H₂O$ co-adsorption, the co-adsorption of both OH and H also enhances the adsorption energy of $CO₂$ by formation of a hydrogen bond between the OH species and one of the O atoms of $CO₂$. For the stable adsorption configurations of $CO₂$ with structures of C(1), C(2) and C(3), corresponding to the co-adsorption configurations DA(1)–DA(3) in [Fig. 5](#page-6-0), the $CO₂$ adsorption energies are increased by 4.8, 2.9 and 8.7 kJ·mol⁻¹, respectively. Nevertheless, the adsorption energies increment of C(2) to DA(2) is smaller than that of co-adsorption with H_2O of C(2) to MA(2). For the most stable co-adsorption configuration of DA(1), this result is almost consistent with the calculation by Yin et al. [\[35\],](#page-11-21) who found that largest binding energy is 50.7 kJ·mol^{-1} without solvation effect. For the adsorption configurations of $CO₂$ in $C(4)$, the adsorption energy has the largest increment by 19.3 kJ·mol⁻¹. Although the adsorption energies of CO₂ in C(1)–C(4) structures increase in varying degrees when dissociative H_2O co-exists, the most stable structure of $CO₂$ adsorption is still $CO₂$ adsorption in $C(1)$ mode, accompanied by H₂O dissociative adsorption with DW(2).

In summary, the main effect of co-adsorption of $H₂O$ in molecular and dissociative states on the adsorption of $CO₂$ on a $K₂CO₃/TiO₂$ sorbent is a slight increase in the stability of the $CO₂$ adsorption on the sorbent. Our results are consistent with Mahinpey et al. [\[28\]](#page-11-14), who explained that the increase in adsorption energy of $CO₂$ is due mainly to the fact that the activated K_2CO_3 ⁻[H₂O]_{ads} basic site might have a much greater affinity for interacting with the acidic $CO₂$ than neutral $K₂CO₃$.

Among the various co-adsorption configurations, the co-adsorption of molecular H₂O or dissociative H₂O and CO₂ makes the weakest CO₂ adsorption enhance in maximum extent compared to the $CO₂$ adsorption alone; however, the strongest adsorption of $CO₂$ is still the one in C(1) whether the co-adsorption of $CO₂$ with molecular H₂O and dissociative H_2O or CO_2 adsorption alone.

3.4. Bicarbonate formation pathway

In our previous work, the formation of bicarbonate may have been facilitated through the "one-step mechanism" and the "two-step mechanism" [\[14\].](#page-11-7) Herein, we also investigated bicarbonate formation reaction through the two mechanisms.

3.4.1. Bicarbonate formation from "one-step mechanism"

Beginning with the most stable co-adsorption configurations for $H₂O$ and CO₂ in M(2), bicarbonate formation requires a path in which the OH dissociates from the H_2O molecule and attacks the adsorbed $CO₂$; the other H in H₂O molecule transfers to the $CO₃$ anion. The optimized geometries of the reactant, transition state (TS) and product are shown in [Fig. 6](#page-7-0), the corresponding transition state structural parameters, reaction activation energy and reaction energy are listed in [Table 4.](#page-7-1) In the transition state (TS), the H-O bond length in the adsorbed H_2O is elongated from 0.984 to 2.481 Å, and the distance

Table 2

Adsorption energies, representative geometrical parameters and the total Mulliken charge of a CO₂ molecule co-adsorbed with a H₂O molecule on K₂CO₃ loaded on $TiO₂$ (1 1 0) surface.

Configurations	r(Ti-O _c) ^a (Å)	r(C-O _b) ^b (Å)	$r(K-Oc)a$ (Å)	$r(HO)$ (A)	$r(C-O)$ (A)	α (OCO) (\degree)	ΔE_{ads} (kJ·mol ⁻¹)	Charge (e)
M1	2.799	2.912	2.911	2.331	1.179, 1.182	177.0	-45.3	-0.04
M ₂	2.096	2.991	3.417	2.743	1.176, 1.181	176.0	-57.9	-0.05
M ₃	2.797, 3.027	$\overline{}$	-	2.371	1.180, 1.183	178.5	-40.5	-0.05
M4	\equiv	2.608	4.323	1.733	1.173, 1.190	174.3	-41.5	-0.01

^a The O_c is refer to O atom of CO₂ molecule.
^b The O_b is refer to a generic surface bridging O atom.

Fig. 5. Top views of the main co-adsorption configurations of CO₂ with a dissociative H₂O molecule over the K₂CO₃ loaded on TiO₂ (110) surfaces. For increased clarity, the oxygen atoms of CO₂ and H₂O are indicated in pink, and the oxygen atoms of the slab are indicated in red. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

between the C atom of $CO₂$ and O atom of $H₂O$ is shortened from 2.910 to 2.108 Å. The calculated values of the activation energy and reaction energy are 146.6 and 66.6 kJ·mol $^{-1}$, respectively. The activation energy is far greater than those on low-index surfaces of monoclinic and hexagonal K_2CO_3 obtained in our previous work [\[14\]](#page-11-7), which are 19.3 to 70.4 kJ·mol−¹ .

3.4.2. Bicarbonate formation from "two-step mechanism"

In our previous work, the "two-step mechanism" involved H_2O dissociating into OH and H, then OH attacking $CO₂$ to form a $HCO₃$ anion, and H combining with $CO₃$ to form HCO₃ [\[14\].](#page-11-7) On the TiO₂supported K_2CO_3 sorbent, there are two areas we will take into account in this study, namely, the surface of $TiO₂$ (110) and the interface of K_2CO_3/TiO_2 (110). Different from pure K_2CO_3 , the H from H_2O dissociation must migrate on the sorbent of K_2CO_3/TiO_2 and then combine with a $CO₃$ anion to form a $HCO₃$ anion, rather than combining directly with $CO₃$ in the sorbent to form $HCO₃$. Therefore, the "two-step mechanism" includes an additional process of H migration besides the aforementioned two steps, as opposed to that on a pure K_2CO_3 sorbent.

3.4.2.1. H_2O dissociation. Starting from the stable adsorption of H_2O on the surface with structures of $W(1)$ and $W(2)$, we have analyzed the dissociation of the H₂O molecule. The dissociated H₂O molecule leads to the formation of a terminal hydroxyl (OH_t) and a bridging hydroxyl (OH_b) , as shown in DW(1) and DW(2) in [Fig. 3,](#page-4-0) and the structures of the transition state are shown in [Fig. 7](#page-8-0), the corresponding transition state structural parameters, reaction activation energy and reaction energy are listed in [Table 5.](#page-8-1) The resulting activation energy and reaction energy obtained from calculations using a transition searching method are 48.2 and 8.7 kJ·mol⁻¹ from W(1) to DW(1), and 37.6 and -13.5 kJ·mol⁻¹ from W(2) to DW(2). The results show that H₂O dissociation at the interface of K_2CO_3/TiO_2 has a relatively low reaction barrier and that the reaction process is exothermic, indicating that it is easy to dissociate H_2O at the interface of $K_2CO_3/$ TiO₂. Although H₂O dissociation on the surface of TiO₂ also has low activation energy, the reaction is endothermic. The entire process from adsorption of H_2O to dissociation into OH and H is exothermic and of a low heat entropy change. We therefore believe that H₂O is also easy to

dissociate on the surface of $TiO₂$.

From the above results, one can conclude that the adsorption of H_2O in molecular states is easy to dissociate, whether H_2O adsorbed at the interface of K_2CO_3/TiO_2 or on the surface of TiO₂. Further, because of the lower activation energy at the interface of $\text{K}_2\text{CO}_3/\text{TiO}_2$ compared to that on the surface of TiO₂, one can conclude that the presence of K_2CO_3 on TiO₂ promotes the dissociation of H₂O, which is similar to the conclusion obtained by Grinter et al. [\[51\]](#page-11-34) that a more favorable H_2O dissociation is fostered by the presence of K atoms on the surface. On the other hand, the activation energy of $H₂O$ dissociation at the interface of K_2CO_3/TiO_2 sorbent is lower than that on pure K_2CO_3 (55.0 kJ·mol⁻¹) [\[14\]](#page-11-7), indicating that the support TiO₂ not only facilitates K_2CO_3 dispersion, but also makes H_2O dissociation easier.

3.4.2.2. H proton transfer. Based on the dissociative configurations of DA(1) and DA(2), the calculated result shows that the reaction of the H proton cannot combine directly with $CO₃$ anions, as that on a pure $K₂CO₃$ sorbent. Therefore, H transfer is dispensable for the mechanism. The direct H transfer from OH_b to the O atoms of $CO₃$ anions is unfavorable due to the greater distance of H proton transfer. Taking into account the presence of $H₂O$ molecules in this situation, we think that H2O molecules can also participate in this process, as shown in [Fig. 8](#page-8-2), the corresponding transition state structural parameters, reaction activation energy and reaction energy are listed in [Table 6](#page-8-3).

The resulting activation energies and reaction energies are 54.0 and 19.3 kJ·mol−¹ for DA(1) to P1 via TS2-2-1, and 59.8 and −8.7 kJ·mol−¹ for DA(2) to P2 via TS2-2-2, respectively. The calculated results confirmed that the presence of the H_2O molecule makes the H transfer possible.

3.4.2.3. OH_t reaction with CO_2 . We explored the bicarbonate formation reaction mechanism by reacting $CO₂$ and OH_t based on the coadsorption configuration of $CO₂$ and OH in DA(1) and DA(2) structures. The calculated reaction pathways of the $CO₂$ and OH are shown in [Fig. 9,](#page-9-0) the corresponding transition state structural parameters, reaction activation energy and reaction energy are listed in [Table 7,](#page-9-1) wherein the reaction refers to the OH_t attacking nearby $CO₂$ molecules adsorbed at the Ti site. The resulting activation energies are

Table 3

Adsorption energies, representative geometrical parameters and variation of the total Mulliken charge of a CO₂ molecule co-adsorbed with a dissociative H₂O molecule on K_2CO_3 loaded on TiO₂ (1 1 0) surface.

Configurations	r(Ti-O _c) ^a (Å)	$r(O_b-C)^b$ (Å)	$r(K-O_c)^a$ (Å)	r $(HO_c)^a$ (\AA)	$r(C-O)$ (A)	α (OCO) (\degree)	ΔE_{ads} (kJ·mol ⁻¹)	Charge (e)
DA1	2.839	2.934	2.888	2.576	1.177, 1.183	177.0	-48.2	-0.04
DA ₂	2.690	3.021	3.506	2.497	1.175, 1.184	177.7	-43.4	-0.07
DA3	3.070, 2.784	$\overline{}$	$\overline{}$	2.508	1.180, 1.182	178.6	-40.5	-0.05
DA4	$\overline{}$	2.671	4.245	1.763	1.175. 1.187	175.0	-42.5	-0.03

^a The O_c is refer to O atom of CO₂ molecule.
^b The O_b is refer to a generic surface bridging O atom.

44.4 and 57.9 kJ·mol⁻¹, respectively. Meanwhile, the processes are

slightly exothermic, with reaction energies of −7.7 and −28.9 kJ·mol−¹ . Obviously, the reaction barrier is slightly lower on the surface of TiO₂ than on the interface of K_2CO_3/TiO_2 . Our calculated activation energy on the surface of $TiO₂$ is almost equal to that $(48.2 \text{ kJ·mol}^{-1})$ on clean TiO₂ [\[35\],](#page-11-21) and higher than that $(25.1 \text{ kJ·mol}^{-1})$ on pure K₂CO₃ [\[14\]](#page-11-7).

The activation energies in the above elementary reactions are similar, which leads to difficulty in judging the carbonate performance. Therefore, the microkinetic modeling for the CO_2 capture on $K_2CO_3/$ $TiO₂$ will be investigated, and the rate of bicarbonate formation is then calculated at each site.

3.5. Microkinetic modeling

For the "one-step mechanism", only reactions at the interface of K_2CO_3/TiO_2 were taken into account. The corresponding activation free energies G_a , reaction free energies ΔG and rate constant k are summarized in [Table 8](#page-9-2) (R1, R2 and R6).

Reactions [\(1\) and \(2\)](#page-2-0) (R1 and R2) are presumed to represent equilibrium, with equilibrium coverages of $CO₂$ and $H₂O$ determined as a function of partial pressures, and assuming competitive Langmuir adsorption and excluding possible other adsorbed species, such as bicarbonate.

These were calculated by the following formula:

$$
\theta_{\text{H}_2\text{O}} = \frac{K_{\text{H}_2\text{O}} P_{\text{H}_2\text{O}}}{1 + K_{\text{H}_2\text{O}} P_{\text{H}_2\text{O}} + K_{\text{CO}_2} P_{\text{CO}_2}}
$$
(11)

$$
\theta_{\rm CO_2} = \frac{K_{\rm CO_2} P_{\rm CO_2}}{1 + K_{\rm H_2O} P_{\rm H_2O} + K_{\rm CO_2} P_{\rm CO_2}}\tag{12}
$$

The equilibrium constants for $CO₂$ and $H₂O$ adsorption were estimated by the formula [\[47\]:](#page-11-30)

$$
K = \exp[-(E_{ads} - T\Delta S)/k_B T] \tag{13}
$$

where ΔS is the entropy change of gas-phase CO₂ or H₂O, which are obtained from NIST Chemistry Web Book. The reaction rate r for bicarbonate formation (R6) at each site was calculated by the following formula:

$$
r_6 = k_6 \theta_{\text{H}_2\text{O}} \theta_{\text{CO}_2} \tag{14}
$$

The Gibbs adsorption free energy, equilibrium constant of $CO₂$ and H2O are listed in [Table 9](#page-9-3), with all reaction conditions at 350 K; a gas mixture of 0.15 atm CO_2 , 0.15 atm H₂O, and 70% N₂, and a total Fig. 6. The pathways for reaction of co-adsorption configurations of $CO₂$ and $H₂O$ species M(2). For increased clarity, the oxygen atoms of OH_t and $H₂O$ are indicated in pink, and the oxygen atoms of the slab are indicated in red. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

pressure of 1 atm were considered [\[15\].](#page-11-8)

The Gibbs free energy of CO_2 adsorption is less than that of H_2O , so the $CO₂$ adsorption equilibrium constant is exceedingly smaller than that of H₂O. The calculated reaction rate constant k , θ_{CO_2} , $\theta_{\text{H}_2\text{O}}$, and reaction rate are 2.06×10^{-10} s⁻¹, 8.25×10^{-8} , 0.9999 and 1.70×10^{-17} s⁻¹, respectively. The reaction rate for bicarbonate formation from $M(2)$ is small due to the smaller reaction rate constant k and coverage of CO_2 , θ_{CO_2} . This is similar to bicarbonate formation on a K_2CO_3 (0 0 1) surface obtained by Gao et al. [\[32\]](#page-11-18), who found that the reaction rate for bicarbonate formation is small because the $CO₂$ adsorbed fraction is very small. We also calculated the reaction rates on the low index on pure K_2CO_3 based on our previous investigation, listed in [Table 10.](#page-10-0) Obviously, the carbonation reaction has the largest reaction rate on the (0 0 1) − 1 surface of K_2CO_3 with a hexagonal structure, which is 9.39×10^7 s⁻¹, far more than that on a K₂CO₃/TiO₂ surface. These results indicate that bicarbonate formation is not feasible at the interface of K_2CO_3/TiO_2 through the reaction with "one-step mechanism".

For the "two-step mechanism" (i.e., H_2O dissociates preceding bicarbonate formation, then proton H transfers to $CO₃$ anions, and OH group from the H_2O dissociation reacts with the gas molecule of $CO₂$), all reactions used for calculation are summarized in [Table 5](#page-8-1) (R2–R5). As OH was found in the carbonation reaction, we therefore first considered H₂O adsorption and dissociation. Reaction (2) (R2) was supposed to be equilibrium. The other step, R3, was described by the forward rate. The site balance of intermediate species included in the reaction mechanism can be written in terms of coverage (θ_X ; X = surface species) for reactions [\(2\) and \(3\).](#page-2-1)

$$
\theta_{\text{H}_2\text{O}} + \theta_{\text{H}} + \theta_{\text{HO}} + \theta^* = 1 \tag{15}
$$

The θ^* is the coverage of vacancy. The coverage of H_2O is calculated as follows:

$$
\theta_{\rm H_2O} = P_{\rm H_2O} K_{\rm H_2O} \theta^* \tag{16}
$$

The θ_H and θ_{HO} can be calculated according to the formula below:

$$
\theta_{\rm H} = \theta_{\rm HO} = k_3 \theta_{\rm H2O} \theta^* \tag{17}
$$

By putting Eqs. [\(16\) and \(17\)](#page-7-2) into [\(15\)](#page-7-3), we can calculate θ^* and surface coverage of other species according to the equilibrium-state approximation presented as follows:

$$
P_{H_2O}K_{H_2O}\theta^* + 2k_3P_{H_2O}K_{H_2O}\theta^*\theta^* + \theta^* = 1
$$
\n(18)

According to these equations, we can obtain the result of θ_{HO}. So the carbonation reaction (R5) rate on per site could be calculated by the

Table 4

Transition state structure parameters, activation energies E_a and reaction energies ΔE for co-adsorption CO₂ and H₂O reaction on K₂CO₃/TiO₂(1 1 0).

Configuration	$r(C-O)$ (Å)	$r(C-O)$ (Å)	r(H1–O _w) ^a (Å)	r(H2–O _w) ^a (Å)	$r(C-O)$ (A)	$O-C-Oo$	E_a (kJ·mol ⁻¹)	ΔE (kJ·mol ⁻¹)
TS1	1.202	1.221	0.981	2.481	2.108	152.3	146.6	66.6

 a The O_w is refer to O atom of H₂O molecule.

Fig. 7. The dissociation of a H₂O molecule over the K_2CO_3 loaded on TiO₂ (110) surfaces.

Table 5

Transition state structure parameters, activation energies E_a and reaction energies ΔE for H₂O dissociative on K₂CO₃/TiO₂ (110).

Table 6

Transition state structure parameters, activation energies E_a and reaction energies ΔE for reaction of H proton transfer reaction from OH_b group to the O atoms of $CO₃$ anions.

^a The O_w is refer to O atom of HO molecule. b The O_b is refer to a generic surface bridging O atom.

^a The O_w is refer to O atom of CO₃ species. b The O_b is refer to a generic surface bridging O atom.

 $DA(2)$

 $TS2-2-2$

Fig. 8. The pathways for reaction of H proton transfer reaction from OH_b group to the O atoms of CO_3 anions. For increased clarity, the oxygen atoms of $H₂O$ are indicated in pink, and the oxygen atoms of the slab are indicated in red. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

Table 7

Transition state structure parameters, activation energies E_a and reaction energies ΔE for gas CO₂ and OH_t reaction on K₂CO₃/TiO₂(1 1 0).

^a The O_w is refer to O atom of OH_t molecule.

Table 8

The relevant elementary reactions of bicarbonate formation on the surface of TiO₂ (1 1 0) and at the interface of K₂CO₃/TiO₂ (1 1 0) together with the corresponding activation free energies G_a (kJ·mol $^{-1}$), reaction free energies ΔG (kJ·mol $^{-1}$) and rate constant k (s $^{-1}$) at 350 K.

Table 9

The Gibbs adsorption free energy (kJ·mol⁻¹) and equilibrium constant of $CO₂$ and H_2O adsorption on the K_2CO_3/TiO_2 sorbent at 350 K.

following formula:

 $r_5 = k_5 \theta_{H0} P_{CO_2}$ (19)

The calculated $\theta_\mathrm{H_2O}$, θ_H and θ_HO are 9.96 \times 10^{-1} , 6.81 \times 10^{-5} and 6.82×10^{-5} on the surface of TiO₂ (1 1 0), respectively, while they are

9.74 × 10^{-1} , 1.25 × 10^{-2} and 1.25 × 10^{-2} at the interface of K₂CO₃/ $TiO₂(1 1 0)$. Next, the reaction rate for H₂O dissociation and bicarbonate formation (H transfer and OH group reacting with the gas molecule of CO₂) are calculated by $r_3 = k_3 \theta_{H_2} \theta^*$, $r_4 = k_4 \theta_H$ and $r_5 = k_5 \theta_{\text{OH}} P_{\text{CO}_2}$; the corresponding values are 6.81×10^{-5} , 7.08 and 5.03×10^3 s⁻¹ on the surface of TiO₂ (110), and 1.25×10^{-2} , 1.40×10^{1} and 6.64×10^{4} s⁻¹ at the interface of K₂CO₃/TiO₂ (1 1 0), respectively.

Obviously, the bicarbonate formation reaction rates of R6 are much lower than those of R4 and R5; therefore, it is impossible for bicarbonate formation through the "one-step mechanism". In our previous work $[14]$ on pure K_2CO_3 , the carbonation reaction occurs through both the "one-step mechanism" and "two-step mechanism". Certainly, the mechanism is different from that on pure K_2CO_3 when TiO_2 support exists. It is noted that the step of H transfer appears in the "two-step

Table 10

The equilibrium constant and coverage of CO_2 and H₂O adsorption, rate constant k and reaction rater for CO_2 and H₂O reaction on the monoclinic and hexagonal K_2CO_3 each surfaces through "one-step mechanism", respectively (T = 350 K).

Table 11

The equilibrium constant and coverage of H₂O adsorption, coverage of OH group, rate constant and reaction rate for H₂O dissociation r_3 as well as CO₂ and HO reaction r_5 on the monoclinic and hexagonal K₂CO₃ each surfaces through "two-step mechanism", respectively (T = 350 K).

Surfaces		k_3 (s ⁻¹	k_5 (s ⁻¹)	K_{H2O}	θ_H2O	$\theta_{\rm HO}$	r_3 (s ⁻¹)	r_{5} (s ⁻¹)
Monoclinic	(001) (011)	2.17×10^{-10} 5.56×10^{-6}	8.89×10^{11} 2.25×10^{13}	2.39×10^{15} 9.69×10^{10}	1.00 1.00	6.06×10^{-25} 3.83×10^{-16}	6.06×10^{-25} 3.83×10^{-16}	8.08×10^{-14} 1.29×10^{-3}
Hexagonal	(010)	2.38×10^{4}	2.31×10^{10}	2.18×10^{11}	1.00	7.28×10^{-7}	7.28×10^{-7}	2.52×10^3

mechanism" over $TiO₂$ supported $K₂CO₃$ sorbent compared to that on pure K_2CO_3 sorbent, where H dissociated from H_2O , need not transfer but directly bonds to $CO₃$ to form $HCO₃$. On the other hand, the reaction rates of R3, R4 and R5 are comparable to each other at the interface of K_2CO_3/TiO_2 or on the surface of TiO₂, and the rate-determining steps are likely governed by reaction step R3, i.e., the H_2O dissociation process is the rate-determining step of the carbonation reaction. Ma-hinpey et al. [\[28\]](#page-11-14) proposed an initial rate-determining step is H_2O adsorption step, and the reaction mechanism follows below equations:

K_2CO_3 (s) + H₂ O (g) $\Leftrightarrow K_2 CO_3$ [H₂ O]_{ads} (20)

$$
K_2CO_3[H_2O]_{ads} + CO_2(g) \Leftrightarrow 2KHCO_3(s)
$$
 (21)

However, the detailed reaction is still not clarified about K_2CO_3 ^{[H₂O]_{ads} reacting with CO_2 . Herein, we proposed that the me-} chanism is (1) chemisorbed H_2O is dissociated into OH and H, then (2) OH is combined with physisorbed CO_2 into HCO_3 on the K_2CO_3/TiO_2 sorbent, and at the time, H is transferred through the surface and combined with $CO₃$ from $K₂CO₃$ into HCO₃. Furthermore, the values of reaction rates at the interface are about 3 orders of magnitude higher than the corresponding values on the surface, which indicates that the interface of K_2CO_3/TiO_2 offers better active sites for CO_2 capture. When K_2CO_3 is supported on TiO₂ (110), the carbonation reaction is accelerated compared to that on a pure K_2CO_3 surface under real reaction conditions (the reaction rate on pure K_2CO_3 is listed in [Table 11\)](#page-10-1). Obviously, the addition of a $TiO₂$ support promotes the dissociation of the H2O molecule, which makes the carbonation reaction accelerate, compared to the pure K_2CO_3 surface.

Although the addition of a $TiO₂$ support promotes the dissociation of H₂O, the overall reaction rate is still not increased. Because H_2O dissociation is the rate-determining step, according to our kinetic modeling, accelerating the dissociation of $H₂O$ will further increase the coverage of OH, thus strengthening the capture ability of K_2CO_3/TiO_2 to CO2. The suggestion may be confirmed by the following experiments. For example, $TiO(OH)₂$ has been reported as a great catalytic support for $CO₂$ capture leading to a significant increase of $CO₂$ sorption capacity per unit of K_2CO_3 by a factor of about 37 [\[24\].](#page-11-11) Furthermore, this group confirmed that $TiO(OH)_2$ /tetraethylenepentamine is a good

sorbent for CO_2 capture [\[25\].](#page-11-40) In the real application, it is proposed that adding promote to the K_2CO_3/TiO_2 sorbent which can improve the dissociation rate of H₂O, or pretreating the K_2CO_3/TiO_2 sorbent to create more OH on the surface of the sorbent so that it is accelerated for $CO₂$ capture.

4. Conclusions

The capture of CO_2 using K_2CO_3 loaded on rutile of TiO₂ has been studied using corrected DFT slab calculations. The active sites of $CO₂$ and H_2O adsorption as well as the detail mechanism of CO_2 capture by K_2CO_3/TiO_2 (110), are present. The results show that, over the K_2CO_3 supported on a (4×2) TiO₂ (1 1 0) surface, CO₂ and H₂O prefer to adsorb at the interface between the $TiO₂$ and $K₂CO₃$. Meanwhile, their adsorptions are weaker than those on pure K_2CO_3 . The H_2O , as well as co-adsorbed OH and H species, bind much more strongly than does the $CO₂$ molecule. Further, co-adsorbed H₂O, as well as OH and H species, can slightly increase the adsorption ability of the $CO₂$ molecule on the sorbent, which is similar to the previous research on $CO₂$ and $H₂O$ adsorbed on pure K_2CO_3 surfaces and pure TiO₂ surfaces. The carbonation reaction is processed not via a "one-step mechanism" but via a "two-step mechanism", i.e., the adsorbed H_2O molecule dissociates to form OH_t adsorbed at the top Ti site and H_b species adsorbed at the bridging of the O site. The $CO₃$ anion then deprives the transferred H_b group, at the same time, the gas $CO₂$ molecule reacts with the OH_t group, leading to the production of the bicarbonate group. More importantly, the reaction prefers to occur at the interface of K_2CO_3/TiO_2 , and H transfer step is added when K_2CO_3 is loaded on the support TiO₂ compared that on pure K_2CO_3 .

The kinetic modeling results show that the carbonation reaction is governed by H_2O dissociation. The dissociation of H_2O may limit the carbonation reaction. Therefore, either H_2O -dissociative or high OH coverage support material should be the most promising candidates for maximizing the carbonation performance of a K_2CO_3 -based solid sorbent in practice.

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